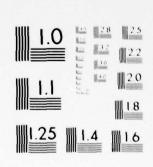
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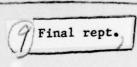
PASSAIC RIVER BASIN
WHITE MEADOW BROOK
MORRIS COUNTY
NEW JERSEY

MT. HOPE LAKE DAM
NJ 00464

SEP 26 1979

PHASE 1 INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

Mt. Hope Lake Dam (NJ-00464)
Passaic River Basin, White Meadow Brook,
Morris County, New Jersey.
Phase 1 Inspection Report.



DACW61-79-C-0011

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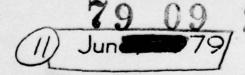
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18. SUPPLEMENTARY NOTES

Copies are obtainable from National Technical Information Service, Springfield, Virginia, 22151.

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Dams embankments structural analysis visual inspection Mt. Hope Lake Dam National Dam Inspection Act report

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Q. ABSTRACT (Continue on reverse side if necessary and identify by block number)

This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report.

NOTICE

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DEPARTMENT OF THE ARMY PHILADELPHIA DISTRICT, CORPS OF ENGINEERS CUSTOM HOUSE-2 D & CHESTNUT STREETS PHILADELPHIA, PENNSYLVANIA 19106

1 2 SEP 1979

Honorable Brendan T. Byrne Governor of New Jersey Trenton, NJ 08621

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Mt. Hope Lake Dam in Morris County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Mt. Hope Lake Dam, a high hazard potential structure, is judged to be in fair overall condition. The dam's spillway is considered inadequate since 77% of the Probable Maximum Flood would overtop the dam. To insure adequacy of the structure the following actions, as a minimum, are recommended.

- a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures, and studies within six months from the date of approval of this report. Any remedial measures necessary to insure the adequacy of the spillway and to prevent overtopping should be initiated within calendar year 1980. In the interim, a detailed emergency operation plan and warning system should be promptly developed. Also, during periods of unusually heavy precipitation, around the clock surveillance should be provided.
- b. Within six months from the date of approval of this report a program should be implemented to regularly observe seepage.
- c. The steel grate walkway over the spillway should be repaired or replaced within three months from the date of approval of this report.

NAPEN-D Honorable Brenden T. Byrne

- d. The following remedial actions should be completed within six months from the date of approval of this report:
- (1) All trees and brush on the embankment should be removed and the dam surface should be properly stabilized.
- (2) The concrete surface of the spillway should be repaired by properly grouting spalls and restoring deteriorated areas and coating with an epoxy sealant.
- (3) Riprap on the upstream face of the embankment should be renovated to provide adequate uniform slope protection.
- (4) The spillway downstream channel should be cleared of significant obstructions.
- (5) The outlet works should be thoroughly inspected and renovated if necessary.
- e. The owner of the dam should initiate a program of periodic inspection and maintenance, the complete records of which should be kept on file. A visual inspection of the dam and appurtenances should be made annually and reported on a standardized check-list form.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman James A. Courter of the Thirteenth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

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NAPEN-D Honorable Brendan T. Byrne

An important aspect of the Dam Safety Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,

1 Incl

JAMES G. TON
Colonel, Corps of Engineers
District Engineer

Collabor LTC

Copies furnished:
Dirk C. Hofman, P.E., Deputy Director
Division of Water Resources
N.J. Dept. of Environmental Protection
P.O. Box CN029
Trenton, NJ 08625

John O'Dowd, Acting Chief Bureau of Flood Plain Management Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CN029 Trenton, NJ 08625

MT. HOPE LAKE DAM (NJ00464)

CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 2 May and 6 June 1979 by Storch Engineers, under contract to the State of New Jersey. The State, under agreement with the U.S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92-367.

Mt. Hope Lake Dam, a high hazard potential structure, is judged to be in fair overall condition. The dam's spillway is considered inadequate since 77% of the Probable Maximum Flood would overtop the dam. To insure adequacy of the structure the following actions, as a minimum, are recommended.

- a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures, and studies within six months from the date of approval of this report. Any remedial measures necessary to insure the adequacy of the spillway and to prevent overtopping should be initiated within calendar year 1980. In the interim, a detailed emergency operation plan and warning system should be promptly developed. Also, during periods of unusually heavy precipitation, around the clock surveillance should be provided.
- b. Within six months from the date of approval of this report a program should be implemented to regularly observe seepage.
- c. The steel grate walkway over the spillway should be repaired or replaced within three months from the date of approval of this report.
- d. The following remedial actions should be completed within six months from the date of approval of this report:
- (1) All trees and brush on the embankment should be removed and the dam surface should be properly stabilized.
- (2) The concrete surface of the spillway should be repaired by properly grouting spalls and restoring deteriorated areas and coating with an epoxy sealant.
- (3) Riprap on the upstream face of the embankment should be renovated to provide adequate uniform slope protection.
- (4) The spillway downstream channel should be cleared of significant obstructions.

- (5) The outlet works should be thoroughly inspected and renovated if necessary.
- e. The owner of the dam should initiate a program of periodic inspection and maintenance, the complete records of which should be kept on file. A visual inspection of the dam and appurtenances should be made annually and reported on a standardized check-list form.

APPROVED:

AMES G. TON

Colonel, Corps of Engineers District Engineer

PHASE I REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam:

Mt. Hope Lake Dam, NJ00464

State Located:

New Jersey

County Located:

Morris

Drainage Basin:

Passaic River

Stream:

White Meadow Brook

Dates of Inspection:

May 2, 1979; June 6, 1979

Assessment of General Condition of Dam

Based on visual inspections, past operational performance and Phase I engineering analyses, Mt. Hope Lake Dam is assessed as being in fair overall condition.

Hydraulic and hydrologic analyses indicate that the spillway is inadequate. The spillway is not capable of passing the designated Spillway Design Flood (SDF) without overtopping the dam. The SDF for Mt. Hope Lake Dam is equal to the Probable Maximum Flood (PMF). The spillway is capable of passing approximately 76 percent of the PMF.

Therefore, the owner should engage a qualified professional engineer in the near future to perform accurate hydraulic and hydrologic analyses relating to spillway capacity. Based on the findings of the analyses, remedial measures should be undertaken to prevent overtopping of the dam resulting from a storm equivalent to the SDF. In the interim, a detailed emergency operation plan and warning system should be promptly developed. Also during periods of unusually heavy precipitation, around the clock surveillance should be provided.

Three zones of seepage are present along the downstream toe of dam. Arrangments should be made soon to monitor the seepage on a monthly basis. The monitoring should be performed by a qualified professional engineer.

The condition of the steel grate walkway over the spillway is hazardous and the walkway should be repaired or replaced soon.

It is further recommended that the following measures be undertaken by the owner in the near future:

 All trees and brush on the embankment should be removed and the dam surface should be properly stabilized. The second secon

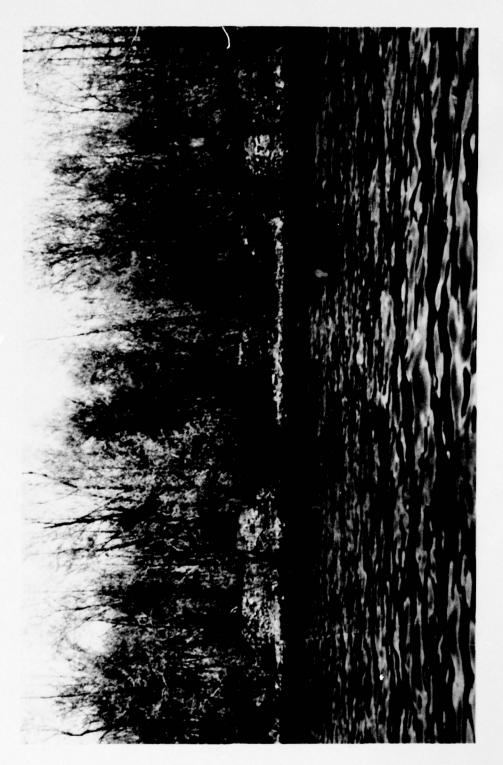
- The concrete surface of the spillway should be repaired by properly grouting spalls and restoring deteriorated areas and coating with an epoxy sealant.
- 3) Riprap on the upstream face of embankment should be renovated to provide adequate uniform slope protection.
- 4) The spillway downstream channel should be cleared of significant obstructions.
- 5) The outlet works should be thoroughly inspected and renovated if necessary.

The owner should, in the near future, implement a program of periodic inspection and maintenance for the dam. Repairs should be made as required and the following maintenance should be performed annually: remove adverse vegetation from the embankment, fill and sod any eroded

surfaces, repair riprap and clear the downstream channel. As part of the maintenance program, the lake should be lowered at least once every five years at which time the lake should be cleaned and normally submerged portions of the dam and spillway inspected and repaired.

Richard J. McDermott, P.E.

John E. Gribbin, P.E.



OVERVIEW - MOUNT HOPE LAKE DAM

2 MAY 1979

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 30214. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that the unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

MT. HOPE LAKE DAM, NJ00464

SECTION 1: PROJECT INFORMATION

1.1 General

A. Authority

Public Law 92-367, August 8, 1972 authorized the Secretary of the Army, through the Corps of Engineers to initiate a National Program of Dam Inspection throughout the United States. The Division of Water Resources of the New Jersey Department of Environmental Protection (NJDEP) in cooperation with the Philadelphia District of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the State of New Jersey. Storch Engineers has been retained by the NJDEP to inspect and report on a selected group of these dams. The NJDEP is under agreement with the Philadelphia District of the Corps of Engineers.

b. Purpose of Inspection

The visual inspections of Mt. Hope Lake Dam were made on May 2, 1979 and June 6, 1979. The purpose of the inspections was to make a general assessment of the structural integrity and operational adequacy of the dam structure and its appurtenances.

1.2 Description of Project

Description of Dam and Appurtenances

Mt. Hope Lake Dam is an earthfill dam with a free overflow concrete and timber weir spillway. The embankment is 1252 feet long with top width of 12 feet. The upstream and downstream faces have slopes of 2.5 horizontal to 1 vertical and 3 horizontal to 1 vertical, respecively. The embankment is generally covered with trees, brush and grass with a foot path located along the crest for its entire length. The upstream slope is protected by dumped riprap. No cut-off structure is shown within the dam on the original design drawing. The spillway is constructed for two staged operation. A primary crest, consisting of a 4-foot long timber flashboard, is located between two concrete weir sections comprising the secondary crest. The concrete secondary crest has a total length of 18 feet and an elevation of 797.0 (N.G.V.D.) while the primary crest is set at elevation 796.5. The overall spillway crest length is 22 feet. A steel grate pedestrian walkway spans the full length of the spillway. The bottom of the walkway is approximately 2.7 feet above the spillway crest.

The crest of dam is at elevation 802.0 and is 5.0 feet (measured vertically) above the secondary crest of the spillway. The maximum height of dam is 18 feet.

The outlet works consists of one 12-inch diameter cast iron pipe with a gate valve located near the discharge end. The outlet works pipe is located approximately 300 feet from the east end of the dam while the spillway is located at the west end of the dam.

b. Location

Mt. Hope Lake Dam is located in the Township of Rockaway,
Morris County, New Jersey. Constructed across White Meadow Brook,
the dam inpounds Mt. Hope Lake which is also known as Mill
Pond. Principal access to the dam is by a local unpaved road.

c. Size and Hazard Classification

Size and Hazard Classification criteria presented in "Recommended Guidelines for Safety Inspection of Dams", published by the U.S. Army Corps of Engineers are as follows:

SIZE CLASSIFICATION

		<u>Impoundment</u>		
Category		Storage (Ac-ft)	Height (Ft)	
Small	<	1000 and \geq 50	$<$ 40 and \geq 25	
Intermediate	≥	1000 and < 50,000	\geq 40 and $<$ 100	
Large	. ≥	50,000	≥ 100	

HAZARD POTENTIAL CLASSIFICATION

Category	Loss of Life	Economic Loss
	(Extent of Development)	(Extent of Development)
Low	None expected (no per-	Minimal (Undeveloped
	manent structures for	to occasional structures
	human habitation)	or agriculture)
Significant	Few (No urban develop-	Appreciable (Notable
	ments and no more than	agriculture, industry
	a small number of	or structures)
	inhabitable structures)	
High	More than few	Excessive (Extensive
		community, industry
		or agriculture)

The following characteristics relating to size and downstream hazard for Mt. Hope Lake Dam have been obtained for this Phase I assessment:

Storage: 1953 acre-feet

Height: 18 feet

Potential Loss of Life:

Three houses are located 300 feet downstream from the outlet works. Dam failure due to overtopping could cause inundation of these structures to a depth of approximately 1 foot above first floor elevation resulting in the potential loss of more than a few lives. Four additional houses are located about 1000 feet downstream from the dam. These structures would be inundated to a lesser extent than would the houses nearer to the dam.

Potential Economic Loss:

Approximately seven houses could sustain water damage as a result of dam failure due to overtopping.

Therefore, Mt. Hope Lake Dam is classified as "Intermediate" size and "High" hazard potential.

d. Ownership

Mt. Hope Lake Dam is owned and operated by Halecrest Corp., Mt. Hope, New Jersey.

e. Purpose of Dam

The purpose of the dam is the impoundment of a lake used for recreation.

f. Design and Construction History

Mt. Hope Lake Dam was designed and constructed in 1944 by the J.G. White Engineering Company. Reportedly, it has not been altered or repaired since that time.

g. Normal Operational Procedures

The dam and appurtenances are maintained by the Halecrest Corp. through its subsidiary company, the Mt. Hope Mining Co. There is no fixed schedule of maintenance; repairs are made as the need arises.

Reportedly, the outlet works is kept in working condition although it has not been used to lower the lake since the dam was originally constructed.

1.3 Pertinent Data

a. Drainage Area

1.9 sq. mi.

The second second

b. Discharge at Dam Site

Maximum known flood at dam site

Unknown

Outlet works at normal pool

10 c.f.s.

Spillway capacity at top of dam

elevation

858 c.f.s.

Elevation (Feet above MSL)

Top of dam	802.0
Maximum pool-design surcharge	802.6
Recreation pool	797.0
Spillway crest - primary crest	796.5
- secondary crest	797.0
Stream bed at center line	
of dam	785.0
Maximum tailwater	801± (at spillway)

d. Reservoir

Length	of	maximum pool	5500	feet
Length	of	recreation pool	4900	feet

e. Storage (Acre-feet)

Recreation pool	633 acre-feet	
Design Surcharge	2138 acre-feet	
Top of Dam	1953 acre-feet	

f. Reservoir Surface (Acres)

307 acres
310 acres
190 acres
190 acres

g. Dam

Туре Earthfill Length 1252 feet Hydraulic height 18 feet Side slopes - Upstream 3 horiz. to 1 vert. - Downstream 2.5 horiz. to 1 vert. Zoning Unknown Impervious core Unknown Cutoff Unknown Grout curtain Unknown

h. Diversion and Regulating Tunnel N.A.

i. Spillway

Type Uncontrolled concrete weir Length of weir - primary 4 feet - secondary 18 feet Crest elevation - primary 796.5 797.0 - secondary Gates N.A. Approach channel N.A. Discharge channel Concrete lined channel

j. Regulating outlets
12" dia.cast iron pipe
with gate valve

SECTION 2: ENGINEERING DATA

2.1 Design

No calculations or reports pertaining to the dam could be obtained. Construction drawings titled "Plan of Proposed Dam and Spillway" by the J.G. White Engineering Company, dated April 2, 1942, are available. The drawings include the following:

- 1. Plan of Dam with Topography
- 2. Profiles of Dam and Spillway
- 3. Sections of Dam and Spillway

2.2 Construction

No data or reports pertaining to the construction of the dam are available.

2.3 Operation

No records of operation of the lake or dam and no inspection reports subsequent to construction are available.

2.4 Evaluation

a. Availability

Available engineering information is limited to the construction plans by J.G. White Engineering Company, on file at Mt. Hope Mining Co.

b. Adequacy

The available engineering information forms a limited description of the subject dam and is considered to be of limited assistance in the performance of a Phase I evaluation. A list of absent information is included in paragraph 7.1.b.

c. Validity

The description of the spillway found on the construction drawings was found to be at variance with observations made during the inspections. Most other information contained on the construction drawings that could be verified is valid within a reasonable allowance for error.

SECTION 3: VISUAL INSPECTION

3.1 Findings

a. General

The inspections of Mt. Hope Lake Dam were performed on May 2, 1979 and June 6, 1979 by staff members of Storch Engineers. A copy of the visual inspection check list is contained in Appendix I. The following procedures were employed for the inspections:

- The embankment of the dam, appurtenant structures and adjacent areas were examined.
- The embankment and accessible appurtenant structures were measured and key elevations determined by surveyors level.

- Key elevations of downstream channel, typical section and elevations of adjacent areas were determined by hand level.
- 4. The embankment, appurtenant structures and adjacent areas were photographed.

b. Dam

The horizontal alignment of the embankment appears to be in conformance with the construction drawings. The vertical alignment of the dam crest is generally level with some irregularity.

The crest of the embankment is partially covered with grass with a bare strip located along its center forming a foot path. Both the upstream and downstream slopes are thickly

wooded with trees and brush and a foot path is worn into the downstream slope at a point near the east end of dam. The upstream slope is protected by riprap along most of its length. The overall condition of the riprap is fair. Variations in the thickness of riprap along the dam were observed.

Adjacent to the downstream toe of embankment, along the west portion of the dam, a ditch or swale containing standing water was observed. The source of the water cannot be determined without further investigation. The swale possibly could have been excavated at the time of original construction to provide fill for the embankment.

Seepage was observed discharging as a trickle from the toe of embankment approximately 25 feet east of the outlet works at a point where a stream flowed prior to the construction of the dam. Orange colored deposits were noted at the discharge point. Two other zones of seepage were observed at the toe of embankment along the west portion of the dam. The seepage was manifest as orange deposits in the standing water.

The generalized soil description of the dam site consists of glacial terminal moraine overlying gneissic bedrock (Byram Gneiss) at or near the surface. The terminal moraine consists of an unassorted and heterogeneous mixture of materials, ranging in size from clay to boulders, deposited at the outer edge of the ice sheet during the Wisconsin stage of continental glaciation.

c. Appurtenant Structures

The concrete overflow section of the spillway is generally in fair condition. The upstream end of the east training wall is

severely spalled and at one location reinforcing rods are exposed. Spalling was also observed on the west training wall near the waterline. The concrete slab forming the spillway crest and apron appears to be in satisfactory condition. Riprap along the spillway section also appeared to be in satisfactory condition. The walkway over the spillway is constructed with a steel grate surface and one section of the grate is absent resulting in a hazardous condition.

The outlet works consists of a 12-inch cast iron pipe with a gate valve. The only component that can be observed is the cover of the steel gate valve casing. The cover which is locked and significantly rusted, did not appear to have been recently removed for gate operation.

d. Reservoir Area

Mt. Hope Lake is an irregularly shaped lake with a maximum width of approximately 4900 feet. The north shore is dominated by structures connected with the Mt. Hope Mining Company. Some homes are located along the west shore of the lake. The overall topography of the reservoir area is wooded with moderate to steep shores having an average grade of 10 percent.

e. Downstream Channel

The spillway discharges into a shallow and winding channel partially obstructed with trees, weeds, rocks and debris. The gradient of the channel increases with distance from the dam and the shape of the channel becomes better defined further downstream. Reportedly, prior to construction of the dam, two streams flowed through the area now occupied by Mt. Hope Lake. After construction, one stream became the spillway downstream channel and the bed of the other stream became the outlet works discharge channel.

SECTION 4: OPERATIONAL PROCEDURES

4.1 Procedures

The level of water in Mt. Hope Lake is regulated naturally by discharge over the spillway of the dam. The lake reportedly is never lowered for any purpose. Reportedly, the gate valve is not opened at times of severe storms to augment the capacity of the spillway.

4.2 Maintenance of the Dam

There is no program of regular inspection and maintenance of the dam and appurtenant structures. Maintenance is performed by the maintenance staff of the Mt. Hope Mining Co. on an "as needed" basis.

4.3 Maintenance of Operating Facilities

Maintenance of operating facilities is performed on an "as needed" basis. The gate valve of the outlet works reportedly is operated every year to confirm that it remains in working condition.

4.4 Description of Warning System

Reportedly, there is no warning system in use at the present time.

4.5 Evaluation of Operational Adequacy

The operation of the dam has been satisfactory to the extent that it has not been known to have overtopped since it was constructed in 1942.

Maintenance documentation is poor and the maintenance program for the dam appears to be insufficient in the following areas:

- 1. Trees and brush on embankment not removed.
- 2. Spalling of spillway training wall not repaired.
- 3. Accumulation of debris in downstream channel not removed.
- 4. Cover on gate valve casing allowed to rust excessively.
- Absent section of steel grate on spillway walkway not replaced.
- Wearing of downstream slope of embankment by pedestrians not corrected.

SECTION 5: HYDRAULIC/HYDROLOGIC

5.1 Evaluation of Features

a. Design Data

Size and hazard classification were used in conjunction with "Recommended Guidelines for Safety Inspection of Dams," published by the U.S. Army Corps of Engineers to establish the SDF (Spillway Design Flood) for Mt. Hope Lake Dam. The appropriate SDF range for this facility is the PMF (Probable Maximum Flood).

The inflow hydrograph for Mt. Hope Lake Dam was calculated using the Soil Conservation Service Triangular Unit Hydrograph with curvilinear transformation and the HEC-1-DB computer program. General hydrologic characteristics used in this method were computed using USGS quadrangles and aerial photographs. The drainage area contributing to Mt. Hope Lake is 1.9 square miles and most of the watershed is undeveloped. The SDF peak was computed to be 11,570 c.f.s.

Reservoir storage capacities were estimated using surface areas measured from USGS quadrangles. Discharge rates for the spillway were computed by the use of a weir formula appropriate for the configuration of its overflow sections. (See Appendix 4). The capacity of the spillway with water level equal to the top of dam was computed to be 858 c.f.s.

The SDF inflow hydrograph was routed through the spillway at Mt. Hope Lake Dam using the HEC-1-DB computer program. For routing analysis, the overall length of the dam with crest elevation at 802.0 (N.G.V.D.) was taken to be 1252 feet. The

routing indicated that the dam would be overtopped by the SDF. The overtopping, in a non-breach condition would occur for about 4.1 hours with a maximum flow height above the dam crest of approximately 0.6 foot and a maximum overall discharge of 2545 c.f.s. The spillway is capable of passing approximately 76 percent of the PMF with lake level equal to the crest of dam.

A breach analysis for the dam was performed using the HEC-1-DB computer program. The breach section was assumed to be located in the area of the outlet works which is the location of maximum height of dam. The analysis indicated that three homes located 300 feet downstream from the dam would be inundated to a depth of approximately 1 foot above their first floor elevation. Four additional homes located 1000 feet downstream from the dam would be inundated to a lesser extent.

The three homes 300 feet downstream from the dam are located along the outlet works discharge channel. Flow in this channel would not exceed 1000 c.f.s. during non-failure conditions since spillway discharge is conveyed by a separate channel. Such a magnitude of flow corresponds to a water level at the three homes approximately 2 feet below their first floor elevation.

Therefore, dam failure due to overtopping would increase downstream flow from a level 2 feet below the first floors of the three homes to a level 1 foot above these first floors. This analysis indicated that dam failure due to overtopping would significantly increase the hazard to loss of life downstream from the dam from that which would exist without overtopping failure.

However, the spillway is capable of passing more than 1/2 PMF with lake level equal to the crest of dam. Accordingly, the subject spillway is assessed as being inadequate in accordance with criteria developed by the U.S. Army Corps of Engineers.

b. Experience Data

Reportedly, Mt. Hope Lake Dam has never been overtopped since it was constructed.

c. Visual Observation

At the time of field inspection there was no evidence of recent overtopping to the dam.

d. Overtopping Potential

As indicated in paragraph 5.1.a, a storm of magnitude equal to the SDF would cause overtopping of the dam to a height of 0.6 foot in a non-breach condition. The spillway is capable of passing approximately 76 percent of the PMF (or SDF) with lake level equal to the crest of dam.

SECTION 6: STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

The embankment appeared at the time of inspection, to be outwardly structurally stable with no evidence of cracks or displacement. However, the visual inspection disclosed three zones of seepage which are described in paragraph 3.1.b. An accurate determination of the severity of the seepage cannot be made without further investigation beyond the scope of a Phase I inspection.

b. Design and Construction Data

Analysis of structural stability and construction data for the embankment and spillway structure are not available.

c. Operating Records

No operating records for the dam are available. A water elevation gage is located near the spillway, but readings have not been recorded since the dam was originally constructed. The water level of Mt. Hope Lake is not presently monitored.

d. Post Construction Changes

Since Mt. Hope Lake Dam was constructed in 1944, no changes or repairs to the dam have been made.

e. Seismic Stability

Mt. Hope Lake Dam is located in Seismic Zone 1 as defined in "Recommended Guidelines for Safety Inspection of Dams" which is a zone of very low seismic activity. Experience indicates that dams in Seismic Zone 1 will have adequate stability under seismic loading conditions if stable under static loading conditions. Mt. Hope Lake Dam appeared to be outwardly stable under static loading conditions at the time of inspection.

SECTION 7: ASSESSMENT AND RECOMMENDATION

7.1 Dam Assessment

a. Safety

Based on hydraulic and hydrologic analyses outlined in Section 5 and Appendix 4, the spillway of Mt. Hope Lake Dam is assessed as being inadequate. The spillway is not able to pass the SDF without an overtopping of the dam.

The dam appeared, at the time of inspection, to be outwardly structurally stable. The seepage is not considered to be an immediate indication of instability. No reported nor written evidence was found that would contradict this assessment.

b. Adequacy of Information

Information sources for this study include: 1) field inspections, 2) plans prepared by the J.G. White Engineering Corp. 3) USGS quadrangle, 4) aerial photograph from Morris County, 5) Consultation with the mine superintendent of Halecrest Corp.

The informaton obtained is sufficient to allow a Phase I assessment as outlined in "Recommended Guidelines for Safety Inspection of Dams."

Some of the absent data are as follows:

- 1. Stream and lake elevation gaging records.
- Maintenance documentation.
- 3. Structural and hydraulic design computations and reports.
- 4. Soils report for the site.
- 5. Seepage analysis and report.

c. Necessity for Additional Data/Evaluation

Additional evaluation is considered necessary in order to assess the effect of the observed seepage on the structural integrity of the dam. The evaluation should be based on monitoring of seepage as outlined in paragraph 7.2.c.

7.2 Recommendations

a. Remedial Measures

Based on hydraulic and hydrologic analyses outlined in paragraph 5.1.a and Appendix 4 the spillway is assessed as being inadequate. Therefore, it is recommended that a qualified professional engineer be engaged in the near future to perform more accurate hydraulic and hydrologic analyses relating to the spillway capacity. The analyses should more accurately determine runoff characteristics of the drainage basin and the downstream channel capacity.

Based on the findings of these analyses, the dam and spillway should be modified to prevent overtopping of the dam resulting from a storm equivalent to the SDF. In the interim, a detailed emergency operation plan and warning system should be promptly developed. Also, during periods of unusually heavy precipitation, around the clock surveillance should be provided.

In addition to the above, it is recommended that the steel grate walkway over the spillway should be repaired or replaced soon.

It is further recommended that the following measures be undertaken by the owner in the near future:

 All trees and brush on the embankment should be removed and the dam surface should be properly stabilized.

- 2) The concrete surface of the spillway should be repaired by properly grouting spalls and restoring deteriorated areas and coating with an epoxy sealant.
- Riprap on the upstream face of embankment should be renovated to provide adequate uniform slope protection.
- 4) The spillway downstream channel should be cleared of significant obstructions.
- 5) The outlet works should be thoroughly inspected and renovated if necessary.

The implementation of the above remedial measures will require proper detailed studies and design and the obtaining of applicable NJDEP approvals.

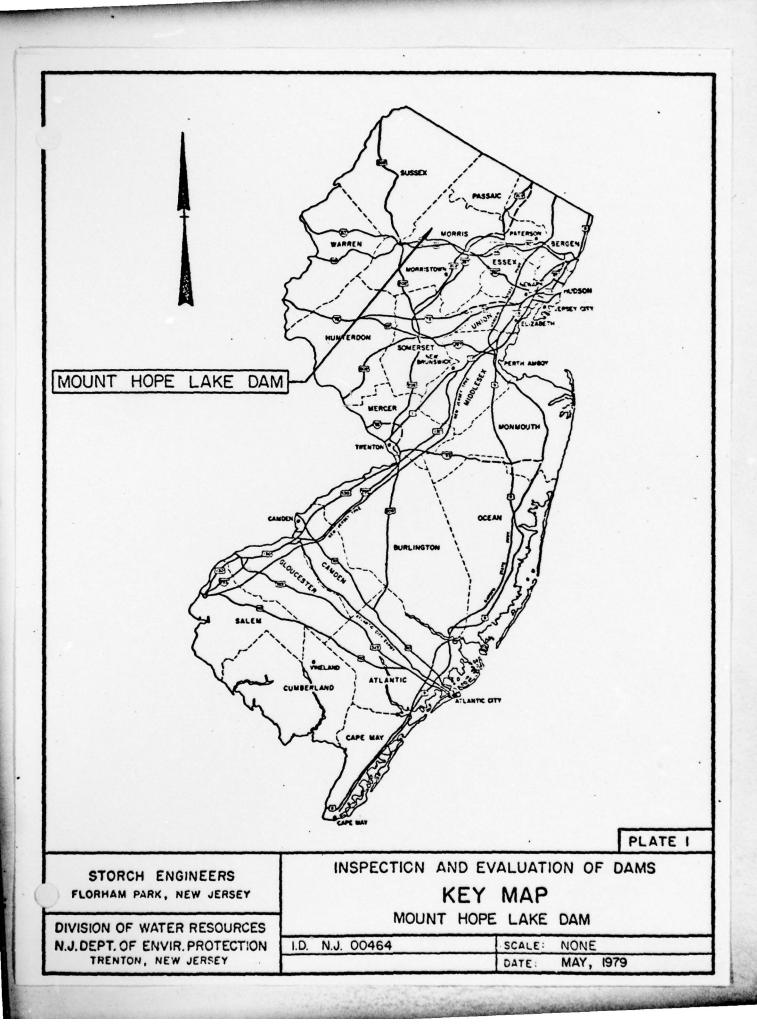
b. Maintenance

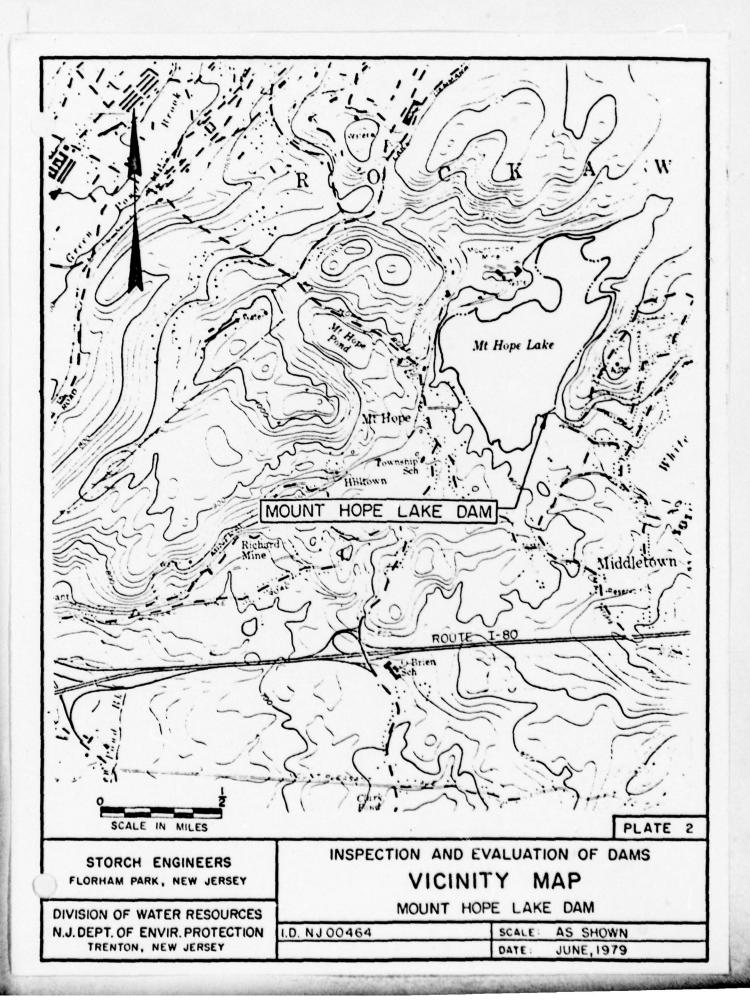
The owner of the dam should initiate, in the near future, a program of periodic inspection and maintenance, the complete records of which to be kept on file and made available to the public. A visual inspection of the dam and appurtenances by a qualified professional engineer should be made annually and reported on a standardized check-list form. Repairs should be made as required and the following maintenance should be performed annually: remove adverse vegetation from the embankment, fill and sod any eroded surfaces of the embankment, repair riprap and clear the downstream channel. In addition, the lake should be lowered at least once every five years at which time the lake should be cleaned and the normally submerged portions of the dam and spillway inspected and repaired.

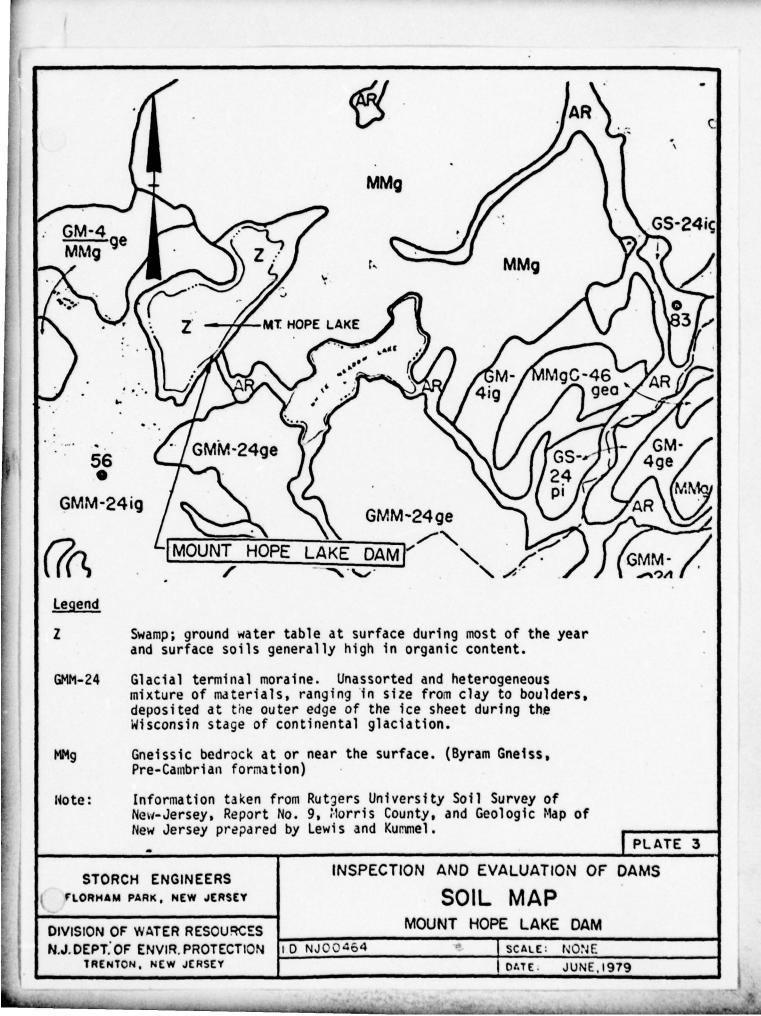
c. Additional Studies

Arrangements should be made soon to monitor the seepage by visual observation. If necessary, measurements should be made by the use of appropriate instrumentation. Standing water in the swale adjacent to the west portion of the dam should be drained prior to performance of the monitoring. The monitoring should be performed on a monthly basis by a qualified professional engineer and included in the permanent records mentioned in paragraph 7.2.b.

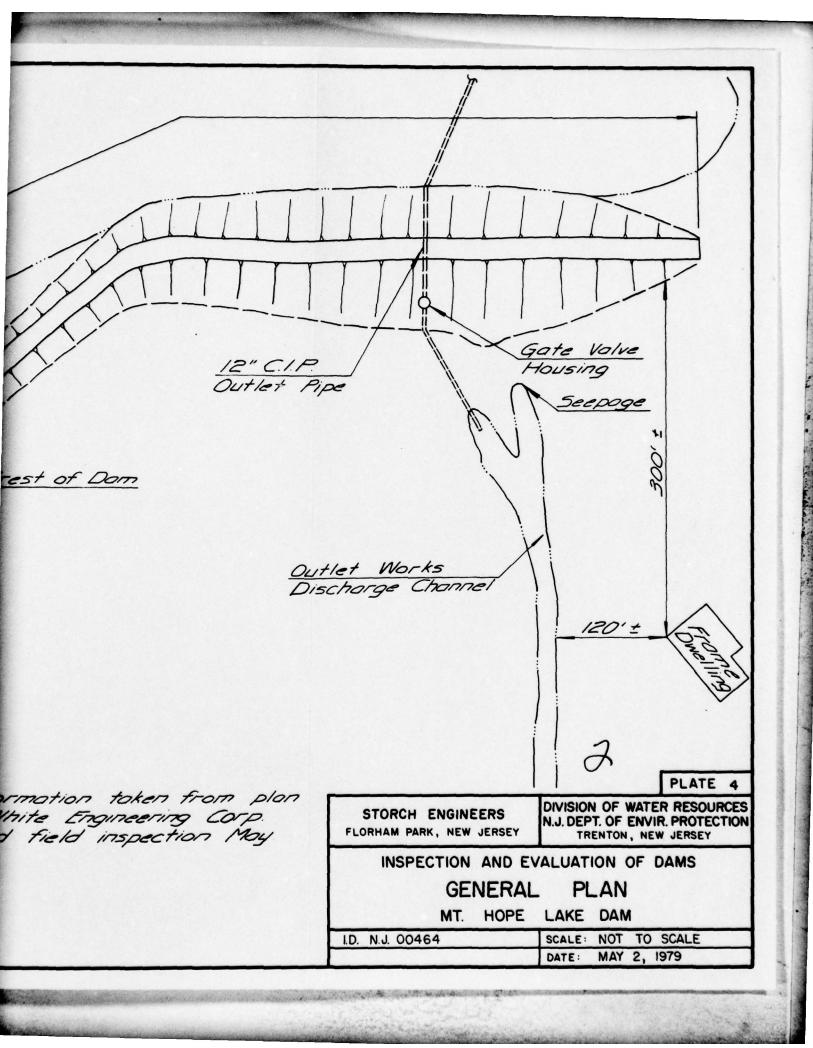
PLATES

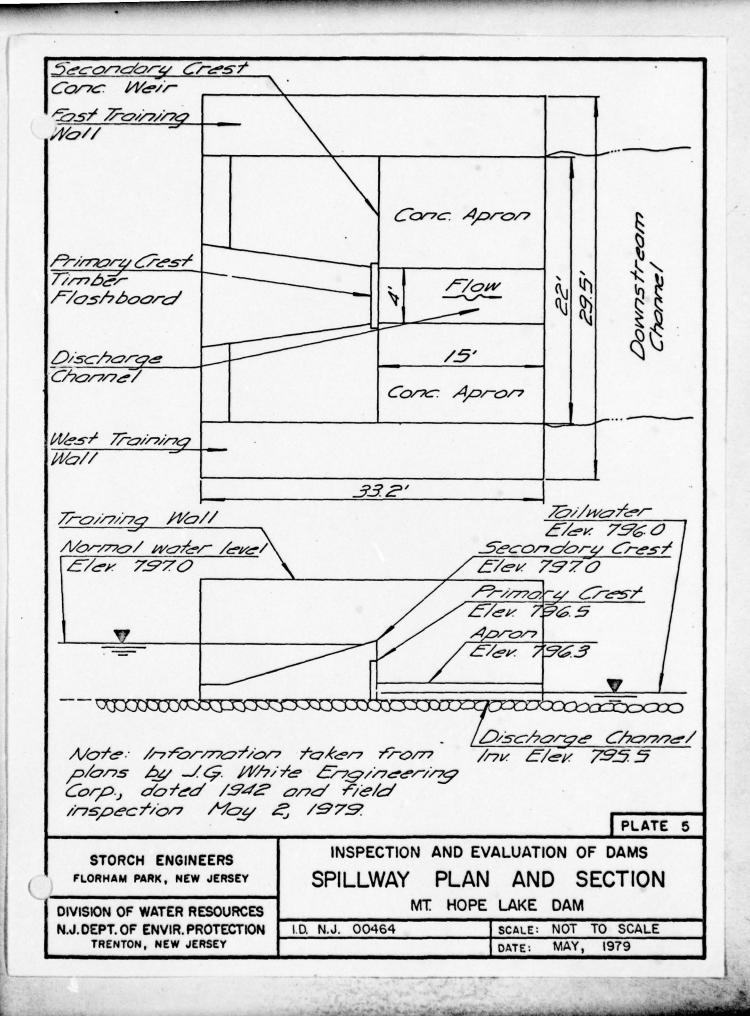


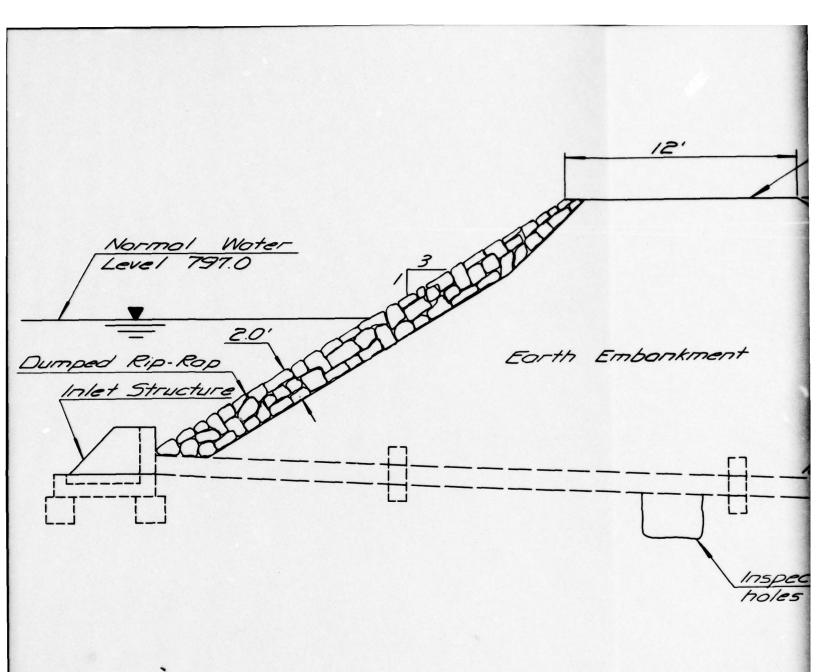




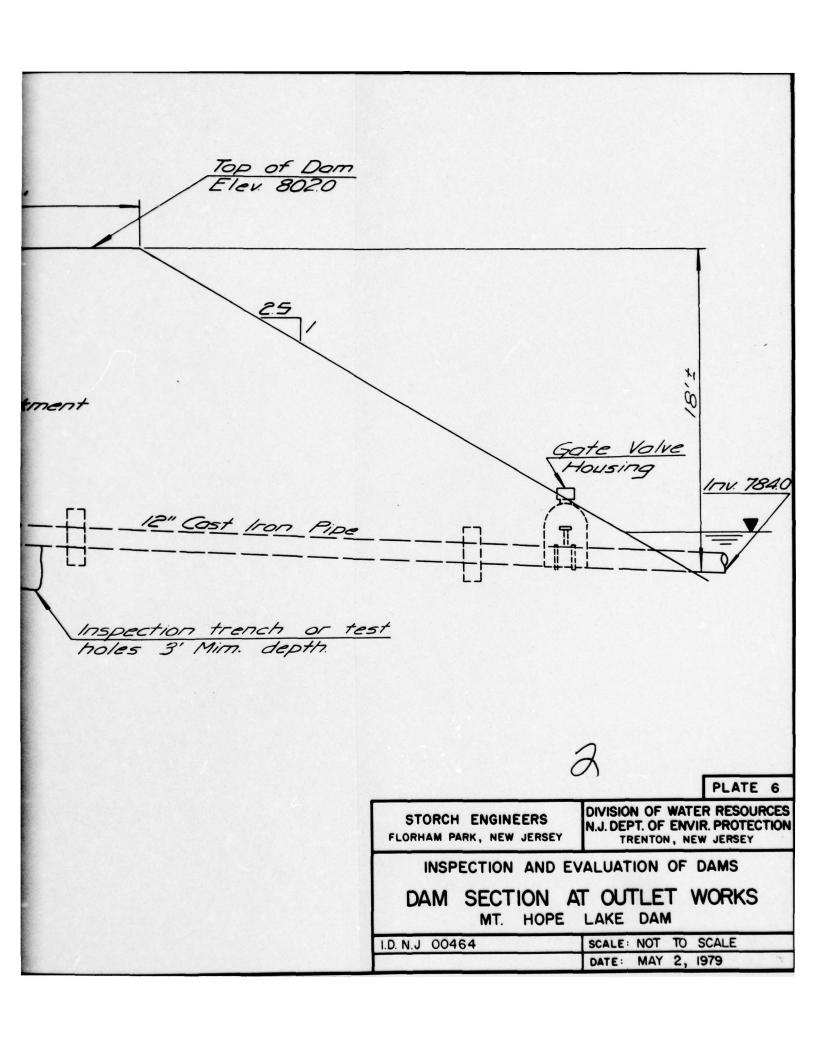
Mt. Hope Loke overall Length = 1252' Dumped Rip-Rop Crest or Spillway Seepage Wet Area Steel Wolkway Note: Information by 16 White Downstream 1942 and field Channel 2, 1979.



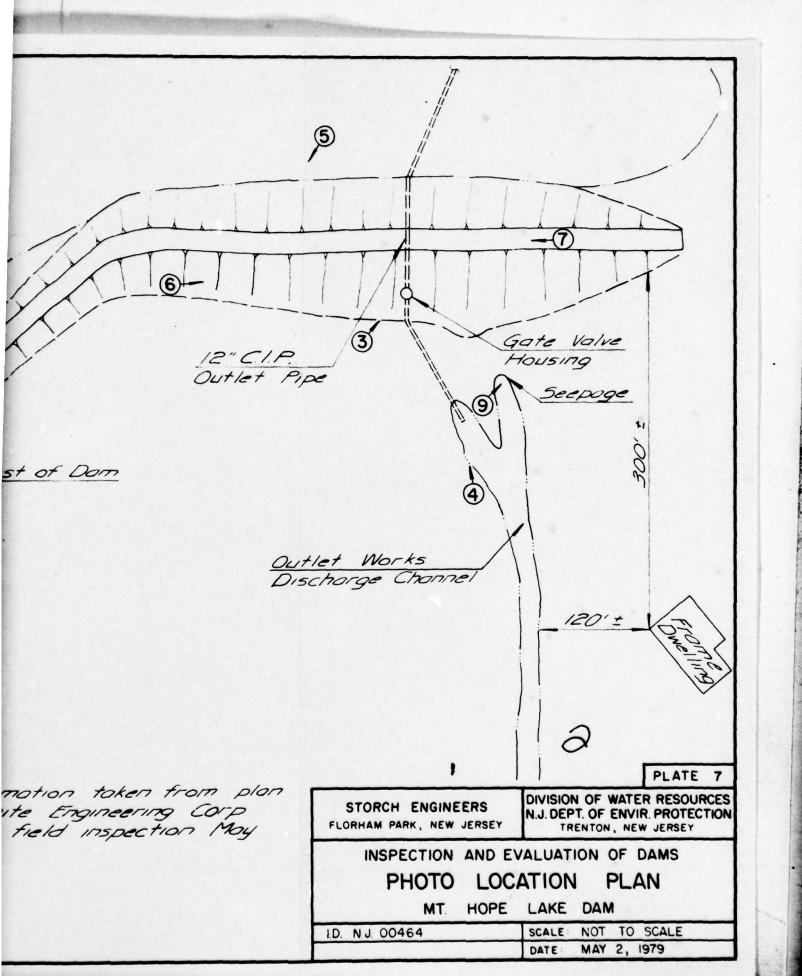




Note: Information taken from plans by J.G. White Engineering Corp., dated 1942 and field inspection May 2, 1979.



Mt Hope Loke Dumped Rip-Rop 2 Crest of D Spillway Seepage Wet Area Steel Wolkway Note Information by 14 White Eng 1942 and field Downstream Channel 2, 1979



APPENDIX 1

Check List - Visual Inspection

Check List - .Engineering Data

Check List Visual Inspection Phase I

Name of Dam Mt. Hope Lake	County	Morris	State New Jersey Coor	Coordinators NJDEP
Date(s) Inspection 5/2/79 6/6/79	Weather	Fair	Temperature 70°F	
Pool Elevation at Time of Inspection 797.0 M.S.L.	on 797.0		Tailwater at Time of Inspection 796.0 M.S.L.	796.0 M.S.L.
Inspection Personnel:				
John Gribbin . Ronald Lai	David Hoyt Joseph Fox		Andrew Miller	
Richard McDermott				
	John Gribbin	in	Recorder	

Present: Charles Penzenik, Mine Superintendent, Halecrest Corp.

CONCRETE/MASONRY DAMS

ISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
ENERAL	N.A.	
TRUCTURE TO BUTMENT/EMBANKMENT UNCTIONS	N.A.	
RAINS	N.A.	
ATER PASSAGES	N.A.	
OUNDATION	N.A.	
ERTICAL AND HORIZONTAL LIGNMENT	N.A.	
		Spinishman and the second of t

CONCRETE/MASONRY DAMS

/ISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS SONCRETE SURFACES	N.A.	
STRUCTURAL CRACKING	N.A.	
CONSTRUCTION JOINTS	N.A.	
AONOLITH JOINTS	N.A.	
EAKAGE	N.A.	
SEEPAGE	N.A.	
	Control My part of the State of the Control Annual	

EMBANKMENT

VISHAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
GENERAL	Embankment covered with dense stand of trees and brush. Foot path located along crest.	Recommend removal of trees.
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	Junction between embankment and concrete spillway appeared satisfactory.	
ANY NOTICEABLE SEEPAGE	Seepage was discharging as a trickle from toe of embankment approz. 25' east of outlet works at point where original stream flowed. Orange deposits noted at discharge point. Two zones of seepage observed at toe of dam as orange deposits in standing water in swale immediately downstream from dam along west portion of dam.	Recommend monitoring of seepage.
STAFF GAGE AND RECORDER	Staff gage immediately upstream from spillway appeared to be in good condition.	Water level at time of inspection at 1.0 foot on gage. Top of scale 3.3 feet.
DRAINS	None observed	

EMBANKMENT

REMARKS OR RECOMMENDATIONS					
OBSERVATIONS	None observed	None observed	No sloughing observed. Erosion on crest of embankment appeared to be due to pedestrian traffic.	Vertical: Generally level (slight variations in elevation) Horizontal: Generally S-shaped - appeared to be aligned true to the construction drawings.	Riprap located along entire length of upstream slope of embankment. Overall condition of riprap is fair. Thickness of riprap coverage varies significantly along embankment. Condition of riprap below water level appears better than that above water surface.
VISUAL EXAMINATION OF	SURFACE CRACKS	UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT . SLOPES	VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	RIPRAP FAILURES

OUTLET WORKS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SURFACES IN OUTLET CONDUIT	M.A.	
INTAKE STRUCTURE	Not observed	Submerged
OUTLET STRUCTURE	Outlet end of pipe obscured by pool. Pipe appeared to be intact.	Submerged in pool of standing water.
OUTLET CHANNEL	Natural streambed of principal stream flowing through lake site prior to construction of dam. 20-foot wide streambed lined with rocks and boulders.	
GATE AND GATE HOUSING	Steel housing protecting gate operating stem was locked and significantly rusted. It did not appear to have been recently operated. Gate and gate housing are buried and could not be observed.	Gate not operated at time of inspection.

SPILLWAY

NS RECOMMENDATIONS	pears to be satis- Conc. weir comprises secondary crest.	Inber flashboard obscured by overflow. Timber flashboard comprises primary crest.	Discharge channel composed of down-stream apron and 4-foot wide channel between apron slabs.	valls are in fair condition. Up- training wall is severely spalled ods exposed. West training wall line.	ire grate surface Absent grate section results in a hazardous condition
OBSERVATIONS	Condition of concrete surface appears to be satis- factory.	Appears to be in satisfactory condition. East slot in concrete weir into which timber flash- board is placed is broken off.	Appears to be in satisfactory condition.	Concrete training walls are in fair condition. stream end of east training wall is severely sprith reinforcing rods exposed. West training spalled near waterline.	Steel walkway constructed with wire grate surface appeared to be structurally adequate. However, one section of grate is absent.
VISUAL EXAMINATION OF	CONCRETE WEIR	TIMBER WEIR	DISCHARGE CHANNEL	GENERAL	WALKWAY

INSTRUMENTATION

VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATICN/SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	None	
PIEZOMETERS	None	
ОТНЕЯ	Staff gage appeared to be in good condition.	

RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS	DEWADYE OF DECOMPOSITION
SLOPES	Slopes surrounding lake range from 2% to 25% with an average slope of approx. 10%.	AETAKAS OK KELUMENDALIONS
SEDIMENTATION	Unknown	
STRUCTURES ALONG BANKS	Structures connected with the Mt. Hope Mining Co. are located along the north shore. A few homes are located along the west shore across a local road,	

DOWNSTREAM CHANNEL

REMARKS OR RECOMMENDATIONS	Recommend clearing of stream.		Area downstream from outlet works is significant hazard area for dam.	
OBSERVATIONS	The spillway downstream channel is a winding shallow natural stream. Trees, weeds, rocks and debris are present in the stream and comprise a significant obstruction to flow.	Banks of stream are generally flat in area of dam. Stream flows through swampy area.	Two homes along spillway downstream channel 1000' A from dam. Three homes along outlet works discharge channel 300' from dam - first floor 9' above channel bottom.	
VISUAL EXAMINATION OF	COMDITION (OBSTRUCTIONS, DEBRIS, ETC.)	SLOPES	STRUCTURES ALONG BANKS	

CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION

ITEM	REMARKS
DAM - PLAN	Plans titled "Plan of Proposed Dam & Spillway" and "Detail of
SECTIONS	Dam and Spillway" prepared by The J. G. White Engineering Co., dated April 2, 1942.
SPILLWAY - PLAN	J. G. White Engineering Co. plans.
SECTIONS	
DETAILS	
OPERATING EQUIPMENT PLANS & DETAILS	J. G. White Engineering Co. plans.
OUTLETS - PLAN	J. G. White Engineering Co. plans.
DETAILS	
CONSTRAINTS	
DISCHARGE RATINGS	
HYDRAULIC/HYDROLOGIC DATA	Not available
RAINFALL/RESERVOIR RECORDS	Not available
CONSTRUCTION HISTORY	Not available
LOCATION MAP	Not available

POST-CONSTRUCTION SURVEYS OF DAM Not available	MATERIALS INVESTIGATIONS Not available BORING RECORDS LABORATORY FIELD	GEOLOGY REPORTS Not available	DESIGN REPORTS Not available	ITEM
		OF DAM	OF DAM	OF DAM

MONITORING SYSTEMS

Staff gage - no records available

MODIFICATIONS

Not available

HIGH POOL RECORDS

Not available

POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS

Not available

PRIOR ACCIDENTS OR FAILURE OF DAM Not available DESCRIPTION REPORTS

MAINTENANCE OPERATION RECORDS

Not available

APPENDIX 2

Photographs

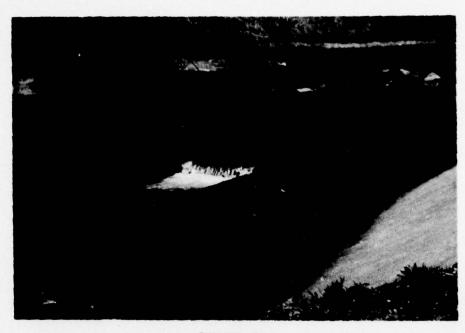


PHOTO 1

DOWNSTREAM VIEW OF SPILLWAY



PHOTO 2
UPSTREAM VIEW OF SPILLWAY



PHOTO 3
OUTLET WORKS OPERATING MECHANISM



PHOTO 4

DOWNSTREAM CHANNEL AT OUTLET WORKS



PHOTO 5
UPSTREAM FACE OF DAM



PHOTO 6

DOWNSTREAM FACE OF DAM



PHOTO 7 CREST OF DAM



PHOTO 8

DOWNSTREAM CHANNEL AT SPILLWAY



PHOTO 9
SEEPAGE NEAR OUTLET WORKS



PHOTO 10

SEEPAGE IN SWALE DOWNSTREAM OF SOUTHWEST SECTION OF DAM

APPENDIX 3

Engineering Data

CHECK LIST HYDROLOGIC AND HYDRAULIC DATA

ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: Mainly wooded
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 797.0 (633 acre-feet)
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): N.A.
ELEVATION MAXIMUM DESIGN POOL: 802.6
ELEVATION TOP DAM: 802.0
SPILLWAY CREST: Concrete and Timber Weir
a. Elevation Primary: 796.5, Secondary: 797.0
b. Type Primary: Timber Flashboard, Secondary: Conc. Weir
c. Width Primary: 4", Secondary: 15' (inclined)
d. LengthPrimary: 4', Secondary: 18'
e. Location Spillover Center of spillway
f. Number and Type of Gates One removable flashboard
OUTLET WORKS: Gated 12" C.I.P.
a. Type Gate Valve in 12" C.I.P.
b. Location 250' from east end of dam
c. Entrance inverts 786.0
d. Exit inverts 784.0
e. Emergency draindown facilities: Open gate to draw down lake
HYDROMETEOROLOGICAL GAGES: One Gage
a. Type Graduated Staff Gage
b. Location Immediately upstream from spillway
c. Records None
MAXIMUM NON-DAMAGING DISCHARGE:
(Lake stage equal to top of dam) 858 c.f.s.

APPENDIX 4

Hydrologic Computations

STORCH ENGINEERS

Sheet _ 1 of _ 10 Project 11+ Hope Lake 2011 Made By 1 Date 5-18-79

Chkd By Dni Date 61

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Hydrologic Analysis

Ronof hydrograph by HEC-1-DB using SCS UHG and routed by The Modified Fuls method. I rainage Area = 1.9 squile

Infiltration Data

Drawinge area is mainly wooded USE initial infiltration 1.5 in constant infiltration 0.15 in/hr.

Time of concentration Byscs TR-55

Cost of serland flow = 1700 ft. = 0.12 bel ef travel = c.9 tt/sec Length of channel flow = 2200 SIODE = 0.03 Vel of travel = 2.5 H/sec

TC = (1700 + 2200) × 1 = 0.77 hr.

Project M+ Hope ake Dans

Made By RL Date 5-18-79

Chkd By Drii Date (17)

Time of concentration of I Zesian of Small Dam"

Cos Nomegraph

Pg 71

H = 240'

L= 3900'

Tc = 0.21 hr.

Time of concentration by Kerby
Pg 14-36
"Handbook of Peplied.
Hydrology" by Chow

tc = 2/3 Lu /5

te = time of concentration in min L = length of overland flow in ft

S = Slope

n = 0.4 Roughness coet.

tc = 28.6 min = 0.48 hr.

to for channel flow 0.24 hr. from

Tc = 0.48 + 0.24 = 0.72 hr.

For HEC - 1 input

Use TC = 0.7 hr. $Lag = 0.7 \times 0.6 = 0.42 \text{ hr}$.

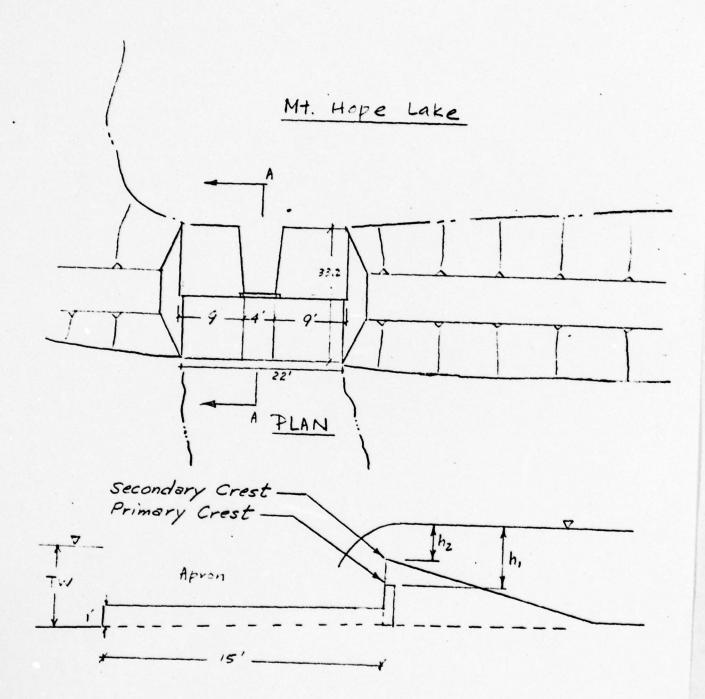
Lake Storage Volume

Information tron USGS 9 Aerial Photos

Elev (11.5.L.)	Surface Area (Ac.)
797	190
800	294
820	420

HEC-1-DB. program will develope Storage capacity from surface area and elev.

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____Made By____C___Date____5-18-79

Chkd By Drir Date (15)79

SPILLIUAY DISCHARGE

Spillway discharge flows over weire at two levels with effective lengths Li and Lz respectively. Lis a broad-crest weir and Lz is a sharp crest weir with triangular section.

Discharge Q can be calculated by
The following tormula:

G = CLINZ C for primary crest 3. Since weir is low and downstream

Channel is shallow, The effect of tailwater is significant. A rough estimate of tailwater elevation is shown on the following page.

These estimates are obtained by using a section 100' downstream and

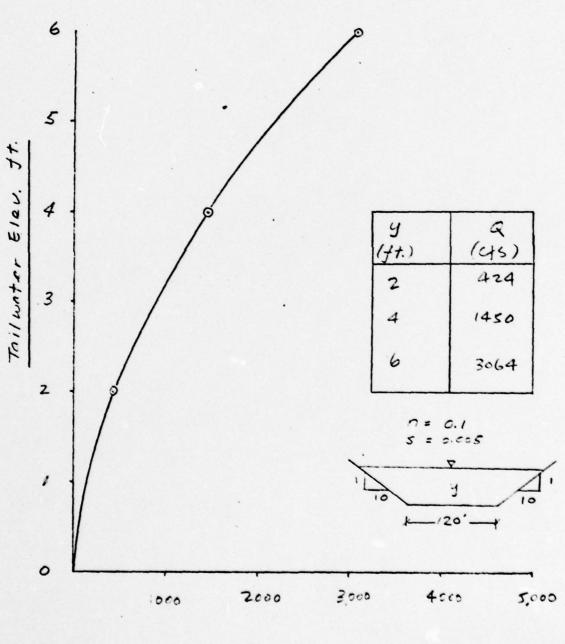
Mannings equation.

Project____

Mit. Hope Lake Dan Made By RL Date 5-15-79

Chkd By Dn? Date Chil

Downstream Channel Tailwater Stage Discharge Curve



a cfs

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Project 11t. Hope Lake Dam Made By RL Date 5-15-79

____Chkd By D111 Date 615/79

Stage Discharge Tabulation

W.L.	h,	12	a,		Tolanter		ZQ
(+)			(ct			adj. tactor	· (cfs)
		•					
796.5	0	0	0	0	-	-	0
797.0	0.5	0	4	0	-	-	4
799.0	2.5	2.0	49	183	7.3	· -	23,2
801.0	4.5	4.0	118	518	2.3	-	636
802.0	5.5	5.0	160	724	2.6	6.97	858
803.0	6.5	6.0	206	952	3.1	0.96	1112
804.0	7.5	7.0	255	1200	3.9	0.95	1.382
805.0	8.5	8.0	307	1466	4.5	0.93	1,649
	•						,

Note: Adjustment tactor applied when weir is submerged
Ref. 5-18 Handbook of Hydraulics King et al.

Sheet 8 of 10

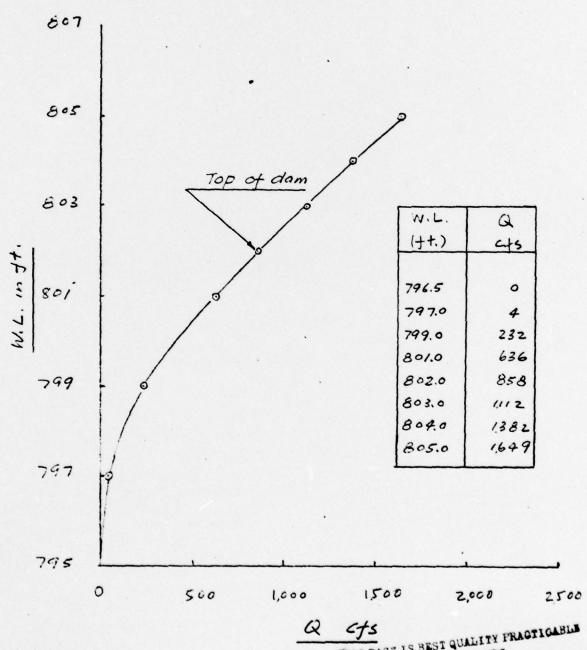
Project 11+ Hoge Loice Dans

Made By RL Date 5-18-77

Chkd By 711 Date 6/5/13

Stage Discharge Curve

Spillway



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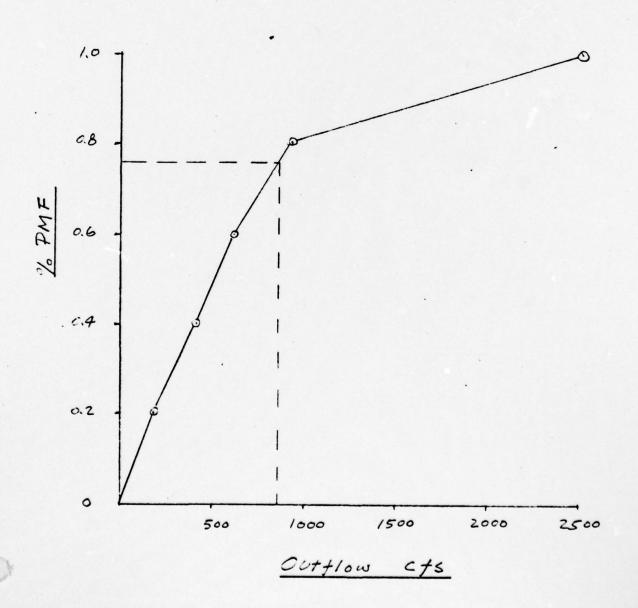
STORCH ENGINEERS

Sheet 9 of 10

Project 14 Hope Lake Dain Made By RL Date 5-22-79

Chkd By DMP Date 6/5/79

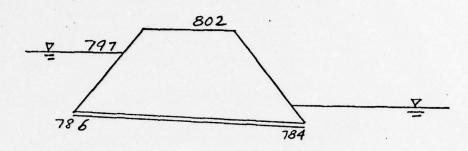
% PMF VS CUTTION



Project Mt Hope Lake Dain

_____Made By___RL__Date___7-31-79

Outlet Works Capacity



12" CIP Outlet control

L=105'

HW = H+1-2

HW = 10

H = 10-1+2= 11 +1.

Using "Hydraulic charts for The Selection of Highway culverts"

Total storage at normal pool 633 Ac-tt $633 \times 43560 = 27,573,480 \quad \text{cu.tt.}$ Average outflow Through pipe = 5 cts $Drawdown time = \frac{27,573,480}{5\times24} \times \frac{1}{3600}$ $= \frac{64}{5} \quad \text{days.}$

HEC-1-DB COMPUTATIONS

0

11	1.0	0.8 LAKE	0.6	0.4	0.2				
1	1 0	25	1NFL 100	OW HYDROI	GRAPH TO	MT. HOPE			
2	-1.0	-0.42 -0.05 DAM	2.0	DISCHAR	0	0	1.5	0.15	
1	796.5	797	799	871	802	803	-797 804	805	
AL	787 796.5	190	232 294 800	636 420 820	858	1112	1382	1649	
0	- 602	2.63	1√5	1252					

SPFE PMS RECIP DATA RAPE RAPE RAPE RAPE RAPE PROGRAM IS .8800 LTK3 RIIOL ERAIN STRKS RIIOK SIRTL CNSTL ALSMX RIIMP 6.00

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1.01	2.35	31	.01	0.00	.01	0.
1.01	2.40	35	• 61	0.00	• 61	3.
1.61	2.50	34	.01	0.00	:01	ő:
1.61	2.55	35	.01	0.00	.01	Ģ.
1.01	3.00	36	-01	0.00	.01	0.
1:01	3.10	38	.01	0.00	:ci	ő.
1.01	3.15	39	.01	0.00	.01	0.
1.01	3.20	40	.01	0.00	•01	0.
1.61	3.30	42	.0 i	0.00	ioi	ŏ:
1.01	3.35	43	.01	3.30	.01	0.
1.01	3.45	45	.01	0.00	-01	0.
1.01	3.50	46	.01	3.00	.01	ŏ.
1.01	3.55	47	•01	0.00	.01	0.
1.01	4.65	49	.01	0.00	-01	0.
1.01	4.10	50	.01	0.00	.01	ō.
1.01	4 - 15	51	.01	0.00	.01	٥٠
1.01	4.25	54	.01	0.00	-01	0.
1.61	4.30	54	.01	0.00	.01	ő.
1.61	4.35	55	•01	0.00	•01	0.
	0111223344550505050505050505050505050505050505	11123456789012345678901234567890123456789012345678901234567890123456777777777777777777777777777777777777		00n630naaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa	• • • • • • • • • • • • • • • • • • •	NNN11111111111111111111111111111111111
1.61	4.50	58	.01	0.00	.01	ŏ.
1.01	4.55	59	• 01	0.00	.01	Q.
1.01	5.05	61	.01	0.00	. 31	0.
1.61	5.10	62	.01	0.30	.01	č.
1.01	5.15	63	.01	0.00	-01	0.
1.01	5.25	65	.01	0.00	.01	0.
1.01	5.30	66	.01	0.00	.01	ö.
1.61	5.35	67	•01	0.00	.01	0.
1:01	5.45	69	.01	0.00	Gi	č:
1.01	5.50	76	•01	0.00	.01	ŏ.
1.01	5.55	71	•01	0.00	-01	Q.
1.01	6-05	75	.33	0.00	.01	0.
1.01	6.10	74	.03	0.00	.03	ŏ.
1.01	6.15	75	.03	0.00	.03	0.
1.61	6.25	77	.03	0.00	.03	8:
1.01	6.30	78	.03	0.00	.03	Ŏ.
1.01	6.35	79	•33	0.30	.03	0.
1.01	6.40	00	•03	0.00	• 0 3	V•

	MO.DA	HR.MN	PERIOD	RAIN	Excs	LOSS	COMP
c	1.01	6.45	81	•03	0.00	•03	
· L	1.0	7.00 7.05 7.10	85 85 86	93 93 93	0.00	03 -03 -03	-
	1.0	7.15 7.20 7.25	87 88 89	- 03	0.00	- 03 - 03 - 03	
' L	1.01	7.35	91	•03 •03 •03	0.00	03	
·	1.01	7.50 7.55 	94 95 96-	.03 .03 .03	0.00	.03	
•	1.01	8.05 8.10 8.15	97 98 99	•03 •03	0.00	.03 .03	
•	1.01	8 · 25 8 · 30 8 · 35	101	03	0.00	.03 .03 .03	
5	1.01	8.45 8.50	105 105	.03	0.00	• 03	
	1.01	9.05 9.05 9.10		. 03	01 01	01	1 3
	1.0	9.15 9.20 9.25	111	•03 •03	:01	:01	
<u> </u>	1:01	9.35 9.40 9.45	115	- 63	- 01 01 01		15
	1.01	9.50	118 119 126	•03 •03	:01	:01 :01	15 16 16 17 17 17 17 17
	1.01	10.10	123	.03	01		17
•	1.01	10.35	125 126 127	.03	•01	.01 .01	18 18 18
	1.01	10.45	129 130 131	.03	.01 .01	.01 .01	18 18 18
_	1.0 1.0 1.6	11.00	133	.03	.01 .01	.01 .01	18 18 18
	11.00000000000000000000000000000000000	666-77-77-77-77-888-88-888-888-999-99-99-99-99-99-99-99	12345678900123456789012345678000000000000000000000000000000000000	\$		033 033 033 033 033 033 033 033 033 033	13 55 80 112 145 116 116 117 117 117 117 118 118 118 118 118 118
	1.01	11.45	139	.03	.01	.01 .01	18 18 18 18
3	1.01	11.50	143	.03	.01 .01 .01	.01	18 18

MO.DA	HR . MN	PERIOD	RAIN	EXCS	LOSS	COMP Q
1.01	12.05	145	:17	-15	.01	208.
1:01	12.05 12.10 12.15 12.20 12.25 12.30	147	:17	15	01	2A2.
1.61	12.25	149		:15	-01	953.
1:01	12.30	150	-17	•15	.01	1232. 1481.
0.00	0.00	152	-:1/-	:15-	001 001 001 001 001 001 001 001 001 001	1686
0.00	0.00	153	•17	.15	.01	1838.
0.00	0.00	155	.17	:15	.01	2028.
0.00	0.00	157	77700000000000005555555555555006393343560053333333333333333333333333333333	19	.01	2141.
0.00	0.00	158	. 20	.19	.01	2193.
0.00	0.00	160	20	19 19 19 19	:0i-	- 2330
0.00	0.00	161	.20	:19	:01	2409.
0.00	0.00	163	• 20	•19	.01	2552.
0.00	0.00	165	.20	19	.01	2646.
0.00	0.00	166	.20	:19	:01	2675.
0.00	0.00	169	.20	- 19-	01-	2713
0.00	0.00	170	.25	.24	:01	2769.
0.00	0.00	171	• 25	- :24	- 01	2830.
0.00	0.00	173	- 25	. 2	.či	3020.
0.00	0.00	175	.25	.24	.01	3210.
0.00	0.00	175	• 25	. 24	- 01	3285.
0.00	0.00	179	25	24	.01	3376.
0.00	0.00	179	- 25	- 24	- 01	3407.
0.00	0.00	161	• 15	.14	.01	3429.
0.00	0.00	183	.30	.29	.01	3398.
0.00	0.00	184	- 46	124499942222222222222222222222222222222	- 01	3432.
0.00	0.00	186	1.29	1.28	.ŏi	4037.
0.00	0.00	189		- 682 -	- :01	6641
0.00	0.00	189	• 53	• 52	-01	8667.
0.00	0.00	191	.30	. 29	.01	11482.
0.00	0.00	193	.23	.22	- 01	10487. 11482.
0.00	0.00	194	. 23	. 22	-01	9825.
	0.00	196-	:23-	- :55		72A2
0.00	0.00	197	. 23	• 22	-01	6328
0.00	0.00	199	. 23	. 22	.01	4993.
0.00	0.00	201	.23	. 55	:01	4216.
0.00	0.00	202	. 23	• 22	- 01	3968.
0.00	0.00	504	- 53-			- 3647.
0.00	0.00	205	• 18	:17	:01	3435.
0.00	0.00	207	-18	•17	.01	3324.
0.00	0.00	209	.18	• 22 • 17 • 17 • 17 • 17 • 17 • 17	.01	3071.
0.00	0.00	210	-18	:17	-01	2948
0.00	0.00	212	.18	.17	.ŭi	2749.
0.00	0.00	214	.18	:17	.01	2633.
0.00	0.00	215	•18	•17	.01	211687. 2188888. 2188888. 2188888. 2188888. 2188888. 218888. 218888. 2
0.00	0.00	217	.01	.00	.01	2530.
0.00	0.00	218	.01	.00	.01	2530 • 2429 • 2234 • 1943 •
- 0.00	0.00	550	· 0 i	- 00 -	.01 .01 .01 .01	1943.
		1444901234567890123456789012345567890123455578901234 1144555555567890123456666667777777777777788888889999990123455578901234 1155555567890123455678901234555789012345557890123455578901234	77777777777777777777777777777777777777	15555555555555555555555555555555555555	0011 0011 0011 0011 0011 0011 0011 001	8.7-4-3. 8.7-7-3.21. 8.7-7-3.21. 9.7-7-3. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3.21. 9.7-7-3. 9.7-7
0.30	0.00	223	:01	• 00	- 01	963.

			2222235353535353544444444455555555556666667777777777	.01 .001 .001 .001 .001 .001 .001 .001		01	5000 - 4000 - 50
	0.00	0.00	227	.ŏi	.00	.ŏi	495.
	0.00	0.00	- 558 -	-:81-		01	462.
	0.00	0.00	229	• 01	• 00	• 61	431.
	0.00	0.00	231	-01	-00	-01	375.
	0.06	0.00 -	_ 232 _	oi -		0i	350-
	0.00	0.00	233	.01	.00	.01	326.
	0.00	0.00	234	•01	• 00	•01	305.
	0.00	0.00	233	- 01	- 00	-01	265-
	0.00	0.00	237	.01	.00	.01	247.
	0.00	0.00	239	.01	.00	.01	231.
	0.00	0.00	239	.01	.00	.01	215.
	0.00	0.00	240 -		- 00		201-
	0.00	0.00	242	-01	-00	-01	175.
	0.00	0.00	243	. ŏi	.00	.01	163.
	0.00	-0.00-	244	01		01-	152.
	0.00	0.00	245	.01 .01 .01 .01 .01 .01 .01 .01 .01 .01	-00	-01	462. 472. 375. 350. 326. 326. 326. 265. 245. 201. 175. 163. 152. 152. 153. 108.
	0.00	0.00	245	• 01	• 00	• 01	133.
-	0.00	0.30	248		- 00		115.
	0.00	0.00	249	.01	.00	.01	108.
	0.00	0.00	250	.01	.00	.01	100.
	0.00	0.00	251	• 01	• 00	•01	94.
	0.00	0.00	253	- Oi	.00	-01	82.
	0.00	0.00	254	.01	.00	.01	76.
	0.00	0.00	255	.01	.00	.01	71.
	0.00	0.00	256	01 01 01 01 01 01 01 01 01 01 01 01		-•6j	66
	0.00	0.00	257	-01	-00	-01	58.
	0.00	0.00	259	.01	.00	.01	54.
	0.00-	0.00	- 260 -	01-		01-	50
	0.00	0.00	261	• 01	-00	• 6 T	•7•
	0.00	0.00	262	-01	• 00	• 01	33:
	0-66	0.60	264	- : : : -			
	0.00	0.00	265	.01	.00	.01	36.
	0.00	0.00	265	-01	.00	-01	33.
	0.00	0.00	261	.01	• 00	• 61	31.
	6.60	0.00	269	.01	-00	-01	27.
	0.00	0.00	270	.01	.00	.01	25.
	0.00	0.00	271	.01	.00	.01	23.
	0.00	0.00	272	01 01 01	- 00-	-01	33
	0.00	0.00	274	-01	-00	-01	19-
	0.00	0.00	275	.01	.00	.01	18.
****	0.00 -	0.00	276	-01-		01	17.
	0.00	0.00	277	.01	• 00	•01	15.
	0.00	0.00	279	- 01	• 00	.01	1::
	0.00	0.00	280	.01 .01 .01		.01	13.
	0.00	0.00	281	.01	.00	.01	12.
	0.00	0.00	282	.01	-00	• 61	12.
	0.00	0.00	283	.01	.00	•01	12.
	0.00	0.00	285	.01	- 00	-01	12.
	0.00	0.00	286	.01	.00	.01	12.
	0.00	0.00	287	-01	.00	-01	12.
-	0.00	0.00	583	• 01	.00	801	151

SU4 (23.40 19.63 3.77 294265. (594.)(499.)(96.)(8332.66)

TOROGRAPH ROUTING

				-	00					1			33	-	:::		:::	+-	.21	mc	189	550	4 8 4	MO	80	SM
	IAUTO			805.00	1649.00								**		•••		:::	-	500	988	931	96.	200	38.	11.	36.
	ISTAGE	LSTR	ISPRAT -1	804.00	1382.00				70.0														M W	90	&	1
	INAME		STORA -	80	138				u				**	1	:::	-	• • • •		200	T -	173	880	315	1076.	CIA	739
	JPRT	0 W d I	15K	803.00-	1112.00				CAREA	04MUID 1252.	RATIO 1	ORDINATES	**		• • •		:::	90	101	83.	O.O.	20	MA	195	0	7430
	JPLT	140	0.000°0						000	DATA EXPO DA 1.5 1	1.				• • •		•••			• •			NN			
RGE THRU DAM		ATA 1	AMSKK 0.000	802.00	858.00	1			ELEVL	COOD DAN	DAM. PLAN	END-OF-PERIOD HYDROGRAPH	70	1	744	•	***	, mc	181	75	- CO 4	00	522	00	SO	746
THRU DAM	1	ROUTING C	AG O.O.	1.00	636.00	•	• •	.0	EXP 0.0			F-PERIO	OUTFLOW 4.	1	• • •		• • •	+ +-	18	# a	EM	100	MO TO	04	52	1788
ROUTE DISCHARGE	P IECON	. I	_	801	63	450.	8456.	820	3000	TOP EL 902.0	STATION	END-0	##	•	• • •		• • •		70.	-	1	10-	-	100	~~	754.
OUTE DI	ICOMP		NSTDL	199.00	232.00	294.	1354.	800.	SPU10														-~	~		
~	ISTAG	CL0SS 0.000	NSTPS	0	0	190.	633.	797.	CREL S				44		144		• • • •	40	9	24	200	360	738 521	23	C:20	755
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				196.50	00.0	• 0	•	787.					**					4.		1.		9.	5.	•••	• •	
				64		AREA=	CAPACITY=	ELEVATIONS												7.3	11	32	240	145	20	120
				STAGE	FLOW	SURFACE AREA=	CAPA	ELEVA						-			•									

mmoral		0-080	0,00	2-15:02									
IN M W W W W	SUMBLE	98653	000000	nurman	200	26666	2000	4666	2000	20000	333553	-	
できるるできること	さまままま	20000	19419	900000 900000	136	70000	2000		77.6	20000	000000		
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בא נא נא נא נא נא נא נא	WWW CALWW	6648	1488C	204050	402	16666	166	999	2000	20000	2000000 200000000000000000000000000000	=	132909
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なるなるなると	ころうしょう	6488C 8488C 848C	8007 8007 10064	10000000000000000000000000000000000000	761	2666	2000	1000		00000	NONT	S	
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SAGAGA	NONTH MAN	6655	000000 0000000000000000000000000000000	2004 EUL	120	20022	2222	2222	2020	NOC 72	**************************************	8	
												OUTFLOW 1	

in a consideration

A1 A2 A3 B 250 B1 J		MT. HOP	NAL DAM E LAKE D F BREACH	SAFETY PAM NE	ROGRAM W JERSEY NNEL ROU	TING			
B 250 B1 5 J 1	. 1	5		i		0	. 0	3	
XI O	LAKE 2 25	INFL	OW HYDRO	GRAPH TO	MT. HOP	E LAKE D	AH	1	
X -1.0	-0.42 -0.05	2.0				1.5	0.15		
K1		ROUTE	DISCHAR	E THEU	DAM .		-		
- Y1 796.5	797	799 232 294 800	801	802 858	1112	-797 804 1382	805 1649		
\$A 0 \$E 787 \$\$ 796.5 \$D 802 \$B 120	190 797 2.63		420 820						
_ K11	i	1.5 792 CH	1252 ANNEL ROI	797 JTING RE	802	1			
71 0.1 76 0.1 77 195	0 . 05 796 788	0.1 60 295	784	796 75 360	160 790 796	0.03 170	788	184	784
1									
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		DAM BREAG	CH DATA			
BRUID	2	DAM BREAK ELBM 792.00	TFAIL	WSEL	FAILEL	
120.	2.00	792.00	1.00	797.00	802.00	

STATION DAM. PLAN 1. RATIO 1

	DA HR.MN		-08		RAPH ORDIN OUTFLO		RAGE	ST .
1.	01 -10 01 -15 01 -20	3	.25 .33	2			633. 633. 633.	79 79 79 79
1	01 30 01 35 01 40	6	.50 58 67				633. 633.	79 79 79
	01 .50 01 .55	1 2 3 4 5 6 7 8 10 11 11 11	1.00	1			633. 633.	79 79 79
	01 1.10 01 1.15 01 1.20	15 15 16 17	1.17	1			633. 633. 633.	79 79 79 79 79 79 79 79 79
1	01 1.30 01 1.35 01 1.40	18 19 20	1.50	1			633. 633. 633.	79 79 79
1.	01 1.45 01 1.50 01 1.55 01 2.00	21	1.75 1.83 1.92 2.00	0		-	633. 633. 633.	79 79 79 79 79 79 79
1.	01 2.05 01 2.10 01 2.15 01 2.20	189 201 223 225 225 226 227 229 230 230 230 230 230 230 230 230 230 230	2.08 2.17 2.25 2.33	. 0			633. 633. 633.	79 79 79
1.	0111225050505050505050505050505050505050	29 30 31 32 33	2.42 2.50 2.58 2.67	0			633. 633. 633.	79 79 79
1.	01 2.45 01 2.50 01 2.55 01 3.00	35	2.75 2.83 2.92 3.00	8			633. 633. 633.	79 79 79 79 79 79 79
	01 3.05 01 3.10 01 3.15	36 37 38 39	3.08 3.17 3.25 3.33	0			632. 632. 632.	79 79 79
1.	01 3.25 01 3.30 01 3.35 01 3.40	41	3.42 3.50 3.58 3.67	0			632. 632. 632.	79 79 79
	01 3.45 01 3.50 01 3.55	45 46 47 48	3.75 3.83 3.92	0			632. 632. 632.	79 79 79 79 79 79 79 79
1.	01 4.05 01 4.10 01 4.15 01 4.20	51 51 53 53	4.08 4.17 4.25 4.33	8			632. 632. 632.	79 79 79
1.	0111225505050505050505050505050505050505	53 54 55 56	7-53-20-87-5	000			313737373737373737373737373737373737373	79 79 79 79 79 79 79 79 79 79
1.	01 4.35 01 4.45 01 4.50 01 4.55	59	4.75 4.83 4.92 5.00	0			632. 632. 632.	79 79 79 79
	01 5.00 01 5.05 01 5.10 01 5.15	61	5.08 5.17 5.25 5.33	8			632. 632. 632.	79 79 79
1	01 5.25 01 5.30 01 5.35	66	5.50 5.58 5.67	0		•	632.	79 79 79
	5.55	71	5.83 5.92 6.00	000			632. 632. 632.	79 79 79
	01 6.10 01 6.15	75	6.25	000			632. 632. 631. 631. 631.	79
	01 6.35 01 6.40	78 79 80	6.50	000			631.	79 79 79
	01 6.50 01 7.00	82	6.83 7.00	000			631. 631. 631.	777777777777777777777777777777777777777
	5.45505050505050505050505050505050505050	669 7712 774 775 777 779 8812 8818 8818 8818 8818 8818 8818 881	56753208753208753208753208753 555556666666666677777777777777777777				666666666666666666666666666666666666666	79 79 79
	01 7.30 01 7.35 01 7.40	91	7.50 7.58 7.67	000			631.	79

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8.10	98	25		8:		- ::		631.		797 797 797
·20	100	.33		0.		1:		631. 631.		797
8 • 25 8 • 30 8 • 35 8 • 40	101 102 103	• 42 • 50 • 58		0:		- ::		631. 631.		797
8.43	104	. 61		0.		1:		631.		797
8.50	106	890087 0087 123320 155320	-	0:		- 1:		631.		797
9.00	108	- 00		.6.				631.		797
	110	-17	-	35. 58.		. 4.		631. 632. 632. 633.		791
9.15 9.20 9.25 9.30 9.35	iiż.	. 33		83.		:		632.		791 791
9.30	112	-50		125.		4:	-	633.	-	797
9.40	116	•58 •67 •75		152.		5.		635.		797
9.45	118	.83		160.		6.		636.		791 791 791
9.55	120 1	.83 .92		171:		7.		638.		797
	121 1	- 17		177. 178.		9.		640.		797
10.15	123	•25		180.		10.		643.		791 791
10.25	125	25 33 42 50		182.		11.		645.		79
10.15 10.15 10.25 10.30 10.45				182. 183. 183.		12.		647.		79
10.45	129 1	•67 •75 •83		183.		14.		650.		791
0.55	131 1	.92		184.		15:		651.	-	797
00050505050505050505050505050505050505	135	.00		184.		16.		653.		797
11:15	135	12532		184.		17.		655.		791
11.20	136 1	• 33		184.		18.		658.		797
11.30	138 1	·50		184.		20.		661.		797 797
1.40	141 1	.67		184.		21.		663.		
1.50	142 1 143 1	.83		184.		23.		664-		797797797797797797797797797797797797797
2.00	144 1	8900123455678900123		184.		24.		665.		79
12.10	146	.17		208. 282. 437.		25.		669.		79
2.20	147 1	.33		674.		27.		669. 672. 675.		79
12.30	149 1 150 1 151 1 152 1 153 1	.50		1232.		32.		688.		79 79 79
2.40	152 1	.67		1481.		41:		697.		19
12.50	153 1	.75		1838.		54.		719. 732. 745.		79
12.55	155 1 156 1	.92		2028.		68.		758.		797
13.05	157 1	· C8		2141-		83.		772.		79
13.15	153 155 156 157 158 159 160	25		2193. 2255. 2330.		98.		801.		79
3.25	161 1	.42		2409.				832.		798
13.35	163	.58		2552.	-	131.		864.		798
13.45	165	.75		2646.		148.		898		798
13.55	167	.92		2697.		164.		932.	an in the second second	798
\$05050505050505050505050505050505050505	169	.08		2734.		181.		967.		798
14.15	170 1	:25		2830.		198.		1003.		798
14.25	172 1	. 33		3020.		215.		1040.		798
14.30	174 1	.50		3121.		224.	-	1060.		798
14.40	176 1	.67		3285.		249.		1100.		799
14.50	178 1	.83		3378.		282.		1143.		799
15.00	180	.00		3429.		314.		1185.		799
15.10	182	:17	-	3416.		345.		1228.		799
15.20	184	.33		3432.		375.		1270.		799
15.25	185	.50		4037.		407.		1315.		799
15.35	187 1	.58		5045.		427.		1343.		800
5.45	189	.75		8667.		486.		1430.		7777777777777777777777777777777777788888
15.55	16123 16625 16645 16667 16667 16677 16677 16777	2087532087520875208752087520875208752087520875		9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-	-	421986451986543952849505077X69862139992 12354567788901235468912467902582728313992		834841 834841		800
16.05	193	-08		10936.		682.		1712.		801
6.15	195	.25		8478.		773.		1837.		801
	146 1			1292.		ROY.		THRE.		801 801

	MO.DA	HR . MN	PERIOD	HOURS	INFLOW	OUTFLOW	STORAGE	STAGE
	1.01	16.35	199	16.58	4993.	1379. 2137.	1991.	802.1
	1:01	16.40 16.45 16.50	200	16.67	4547.	3009.	2011. 2024. 2028.	802.1 802.2 802.2
BEGIN DAM FAILURE		16.50	202	16.83	3968. 3784.	3938. 4895.	2028.	802.2
	1:01	17.00	204	17.00	3647.	5868.	2013.	802.2 802.1 802.0
	1.01	17.05 17.10 17.15	206	17.17	3435.	7898.	1967.	802.0
	1.01	17.15	207 208	17.17 17.25 17.33	3324. 3199.	9064.	1932.	801.9 801.8
AT 16.50 HOURS	1.01	17.20 17.25 17.30 17.35	209	17.42 17.50	3199. 3071. 2948.	11496. 12707. 12213. 11745. 11303.	1888 • 1835 • 1772 •	801.6
	1.01	17.35	241	17.58	2839. 2749. 2681.	12213.	1706-	801.2
	1.01	17.45 17.45 17.50	212	17.67 17.75 17.83	2681.	11303:	1643. 1582. 1524.	801.0
	1.01	17.50	214		2633.	100000	1524. 1469.	800.6
	1.01	17.55 18.00 18.05	216 217 218 219 220 221 222	18.00	2577. 2530. 2429. 2234. 1943.	10488. 10113. 9757. 9415.	1415.	800.2
	1.01	18.10	218	18.08 18.17 18.25 18.33 18.42	2429	9415.	1365.	800.0 799.9 799.7
	1.01	18.10 18.15 18.20 18.25 18.30	219	18.25	2234. 1943.	9080. 8745.	1221.	799.5
	1.01	18.25	221	18.42 18.50	1003.	8408.	1174.	799.4
	1.01	18.32	263		1265. 963.	7726-	1081.	799.2 799.0
	1:01	18.40	224	18.67 18.75	713. 568.	7398	1034.	798.8
	1.01	18.50	226 227	18.83 18.92	530.	6/5/-	945.	798.5
	1.01	18.55				6452.	863.	798.3 798.1 797.9
	1.01	19.05	230	199455875320 199455875320 199455875320 199455875320 199455875320	431.	5872. 5597. 5333.	825. 788.	797.8
	1.01	19.15	231	19.25	375. 350.	5333.	788. 753. 720.	797.6
	1.01	19.20 19.25 19.30	232	19.42	326.	70370	688.	797.3
	1.01	19.35	234 235	19.50	305. 284.	4599. 4375.	658. 629.	797.1 797.0
	1.01	19.40	236 237	19.67	284. 265. 247. 231. 215.	4173. 3978.	601. 575.	796.8
	1.01	19.50	238	19.83	231.	3789.	550.	796.5
	1.01	19.55	239 240	20.00	201.	3608.	526. 503.	796.4 796.3
	1.01	20.00 20.05 20.10	240 241 242	20.08	201. 187. 175.	3266.	481.	796.1
	1.01	20.15	243	20.25	163.	2949.	461.	795.9 795.7
	1.01	20.20	244	20.33	152.	2800 • 2657 •	422.	795.6
	1.01	20.25 20.30 20.35	246	20.42 20.50 20.58	142. 133. 124.	2657. 2521. 2389. 2264.	388. 372.	795.5 795.4
	1.01	20.40	248	20.67	115.	2264.	356.	795.3
	1.01	20.45	249	20.67 20.75 20.83 20.92	108.	2144. 2030. 1921.	342.	795.1
	0.00	0.00	250 251	20.92	94.	1921.	315.	795.0 794.9 794.8
	0.00	0 - 0 0	252 253	21 60	00	1817. 1718. 1624. 1535.	291-	794.7
	0.00	0.00	254 255	21.25	76. 71.	1535.	281.	794.6 794.5
	0.00	0.00	256 257	21.17 21.25 21.33 21.42 21.50 21.58	66.	14704	260.	794.4
	0.00	0.30	25A	21.50	58.	1369. 1293. 1220.	242-	794.3
	0.00	0.00	259 260	21.67		1152	234.	794.2 794.1
	0.00	0.00	261 262	21.67	47.	1087.	219.	794.0 793.9
	0.00	0.00	263	21.83	41.	968.	205.	793.9
	0.00	0.00	264 265 266	22.08	36.	913. 862. 813.	193. 188. 182.	793:4 -
	0.00	0.00	266	22.17	33.	. 813. 767.	188.	793.7
	0-00	0.00	267 268 269 270	22.33	29.	724.	178.	793.5
	0.00	0.00	270	22.50	25.	724. 683. 645.	178. 173. 169.	793.4
		0 00	2/1	22.58	23.		164.	793.4
	0.00	0.00	273	22.75	38. 354. 351. 227. 220. 220. 18.	543.	160.	793.3
	0.00	0.00	275	22.92	18.	485	150:	793.2
	0.000	0.00	272 273 274 275 277 277 278 279	23.00	17. 15. 14. 13. 13.	55435. 4535. 4530. 4530. 388.	153 150 147 144	7933.67 7933.65 7933.65 7933.64 7933.64 7933.63 7933.61 7933.61 7933.61
	0.00	0.00	278	23.17	14.	410.	141. 138. 136. 134.	793.1
	0.00	0.00	280	23.25	13.	368.	136.	793.0
	0.00	0.00	281	23.42	12.	368. 349. 331.	134.	793.0
	0.00	0.00	282 283	23.58	12.	314.	127. 127. 126. 124. 122.	792.9 792.9 792.9 792.8 792.8 792.8
	0.00	0.00	284	23.67	12:	298.	126.	792.8
	0.00	0.00	284 285 286 287	0875530087553008755300 0012545567890012345567890 22222222222222223555555555555555555555	12. 12. 12. 12.	314. 298. 283. 269. 256. 243.	124.	792.8

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NEW JERSEY DEPT OF ENVIRONMENTAL PROTECTION TRENTON F/G 13/2
NATIONAL DAM SAFETY PROGRAM. MT. HOPE LAKE DAM (NJ-00464) PASSA--ETC(U)
JUN 79 R J MCDERMOTT, J E GRIBBIN DACW61-79-C-0011

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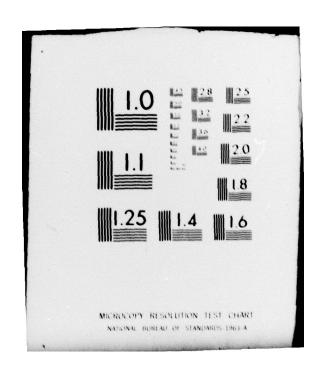
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	SUMMARY OF DAM SAFETY ANALYSIS .											
	ELEVATION STORAGE OUTFLOW	INITIAL TOP	VALUE	SPILL WAY CR 796.50 543. 0.		OF DAM						
RATIO OF PMF	MAXIMUM RESERVOIR WOSOELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW	TIME OF					
1.00 -80 -60 -40 -20	802.50 802.07	.60	2138 · 1976 ·	2545. 944. 633.	1.08	18.06	0:00					
.46 .20	799.85 798.57	0.00	1311. 971.	183.	0.00	18.58	0.00					

		s	UMMARY OF DA	M SAFETY ANA	LYSIS		
•••••	ELEVATION STORAGE OUTFLOW	INITIA 79	7.00 633.	SPILLWAY CRE 796.50 543.	ST TOP	OF DAM 802.00 1953. 656.	
RATIO OF PMF	MAXIMUM RESERVOIR V.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW	TIME OF FAILURE HOURS
1.00	802.24	•24	. 2028.	12707.	77	17.50	16.50
			PLAN 1 MAXIMUM FLOW, CFS	STATION MAXIMUM	TIME		
		RATIO	FLOW, CFS	STAGE .FT	HOURS		
		1.00	12659.	793.4	17.50		

APPENDIX 5

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